



BA-U R 200

BA-U R 200 is top-grade gasket material with special metal reinforcement. Suitable for highest pressure and high temperature applications.

Basis

Aramide fibers, inorganic fillers, NBR, expanded metal reinforcement

DIN 28091-2 FA-A1-St

Colour

Blue

Surface treatment

The standard version has non-stick top and bottom layer. Graphite or PTFE coating on request

Dimensions of standard sheet

Sheet size: 1000x1500 mm 1500x1500 mm

Thickness:

0.8 mm, 1.0 mm, 1.5 mm (other thicknesses available on request)

Tolerances:

Thickness:<1 mm = \pm 0.1 mm, \geq 1 mm = \pm 10%Length: \pm 50 mmWidth: \pm 50 mm

Application

Top quality universal gasket material – specially reinforced - for use at very high pressures, high temperatures and surface stresses. Especially convenient for use at temperature and pressure fluctuations and mechanical vibrations. Due to special metal reinforcement assures also high protection against blow out. Material combines high torque retention, good chemical resistance, excellent sealability and outstanding thermo-mechanical properties. Suitable for sealing of hot water, steam, oils, fuels, non-aggressive chemicals and many other media.

Approvals

Applied for: TA-Luft (VDI 2440), DIN-DVGW (DIN 3535/6)

TECHNICAL DATA

Typical values for a thickness of 1.5 mm

Density DIN 28090-2 g/cm ³ 2.2.2.3 Compressibility ASTM F 36/J $\%$ 5.8 Recovery ASTM F36/J $\%$ >50 Tensile strength - cross grain DIN 52910 MPa $=35$ Specific leak rate DIN 3535/6 mg/(s.m) <0.1 Thickness increase ASTM F146 $ <0.1 \circ Oil IRM 903, 5h, 150°C MAR % <-33 \circ ASTM Fuel B, 5h, 23°C DIN 52913 MPa <-35 Stress resistance 16h, 50MPa,300°C DIN 28090-2 <-35 \circ at room temperature: \varepsilon_{KSW} OIN 28090-2 % <-37 \circ at room temperature: \varepsilon_{KSW} OIN 28090-2 % <-38 Percentage creep deformation DIN 28090-2 <-36 \bullet at elevated temperature: \varepsilon_{KRW} OIN 28090-2 <-36 \bullet at elevated temperature: \varepsilon_{KRW} OIN 28090-2 <-36 <-36 \bullet at elevated temperature: \varepsilon_{KRW} <-36 $				
RecoveryASTM F36/J%>50Tensile strength - cross grainDIN 52910MPa~35Specific leak rateDIN 3535/6mg/(s.m)<0.1	Density	DIN 28090-2	g/cm ³	2.2-2.3
Tensile strength - cross grainDin NoteMPa=35Specific leak rateDIN 3535/6mg/(s.m)<0.1	Compressibility	ASTM F 36/J	%	5-8
Specific leak rateDIN 3535/6mg/(s.m)<0.1Thickness increaseASTM F146• Oil IRM 903, 5h, 150°CM%=3• ASTM Fuel B, 5h, 23°CM%=5Stress resistance 16h, 50MPa, 300°CDIN 52913MPa≈35Compression modulusDIN 28090-27• at room temperature: € _{KSW} M%=7• at elevated temperature: € _{KSW} DIN 28090-2%=8Percentage creep deformationDIN 28090-2%>3• at elevated temperature: € _{KRW} M%≈3• at elevated temperature: € _{KRW} M%≈3	Recovery	ASTM F36/J	%	>50
Thickness increaseASTM F146• Oil IRM 903, 5h, 150°CImage: Comparison of the state of t	Tensile strength – cross grain	DIN 52910	MPa	≈35
• Oil IRM 903, 5h, 150°CImage: Constraint of the system of t	Specific leak rate	DIN 3535/6	mg/(s.m)	<0.1
• ASTM Fuel B, 5h, 23°C• AStress resistance 16h, 50MPa, 300°CDIN 52913MPa ≈ 35 Compression modulusDIN 28090-2• C• at room temperature: ε_{KSW} ≈ -7 ≈ 7 • at elevated temperature: $\varepsilon_{WSW/200°C}$ M ≈ 8 Percentage creep deformationDIN 28090-2 ~ 1 • at room temperature: ε_{KRW} ≈ -7 ≈ 8 Percentage creep deformationDIN 28090-2 ~ 1 • at elevated temperature: ε_{KRW} $\ll -8$ ≈ 1 • at elevated temperature: ε_{KRW} $\%$ ≈ 3 • at elevated temperature: ε_{KRW} \ast $\%$ • Creep deformation 50MPa/300°C- $\%$ • Change in thickness at 20°C $\%$ ≈ 8	Thickness increase	ASTM F146		
Stress resistance 16h, 50MPa,300°CDIN 52913MPa≈35Compression modulusDIN 28090-2• at room temperature: ε _{KSW} %≈7• at elevated temperature: ε _{WSW220°C} %%%≈8Percentage creep deformationDIN 28090-2• at room temperature: ε _{KRW} ODIN 28090-2• at elevated temperature: ε _{KRW} ODIN 28090-2• at elevated temperature: ε _{KRW} %>3• at elevated temperature: ε _{KRW} %≈1• at elevated temperature: ε _{KRW} %≈1• Creep deformation 50MPa/300°C-%≈8• Change in thickness at 20°C%%≈8	• Oil IRM 903, 5h, 150°C		%	≈3
Compression modulusDIN 28090-2 \sim • at room temperature: \mathcal{E}_{KSW} \sim $\%$ \approx 7• at elevated temperature: $\mathcal{E}_{WSW/200^{\circ}C}$ $\%$ \approx 8Percentage creep deformationDIN 28090-2 \sim • at room temperature: \mathcal{E}_{KRW} \sim $\%$ • at elevated temperature: \mathcal{E}_{KRW} \sim $\%$ • at elevated temperature: $\mathcal{E}_{WRW/200^{\circ}C}$ $\%$ \sim • at elevated temperature: $\mathcal{E}_{WRW/200^{\circ}C}$ \sim $\%$ • Change in thickness at 20°C $\%$ \sim	• ASTM Fuel B, 5h, 23°C		%	≈5
• at room temperature: \mathcal{E}_{KSW} Image: Constraint of the sector of the	Stress resistance 16h, 50MPa,300°C	DIN 52913	MPa	≈35
at elevated temperature: $\varepsilon_{WSW/200^{\circ}C}$ M ≈ 8 Percentage creep deformationDIN 28090-2 ~ 8 • at room temperature: ε_{KRW} ~ 6 ~ 3 • at elevated temperature: $\varepsilon_{WRW/200^{\circ}C}$ ~ 6 ~ 1 • Creep deformation 50MPa/300°C- ~ 6 • Change in thickness at 20°C ~ 6 ~ 8	Compression modulus	DIN 28090-2		
Percentage creep deformation DIN 28090-2 • at room temperature: ε _{KRW} % • at elevated temperature: ε _{WRW/200°C} % Creep deformation 50MPa/300°C - • Change in thickness at 20°C %	 at room temperature: ε_{κsw} 		%	≈7
• at room temperature: ε _{KRW} • I>3• at elevated temperature: ε _{WRW200°C} %≈1Creep deformation 50MPa/300°C-• Change in thickness at 20°C%≈8	 at elevated temperature: ε_{wsw/200°C} 		%	≈8
• at elevated temperature: € _{WRW/200°C} % ≈1 • Creep deformation 50MPa/300°C - ~ • Change in thickness at 20°C % ≈8	Percentage creep deformation	DIN 28090-2		
Creep deformation 50MPa/300°C - • Change in thickness at 20°C % ≈8	 at room temperature: ε_{κRW} 		%	>3
Change in thickness at 20°C % ≈8	 at elevated temperature: ε_{wRW/200°C} 		%	≈1
	Creep deformation 50MPa/300°C	-		
Change in thickness at 300°C % ≈10	Change in thickness at 20°C		%	≈8
	Change in thickness at 300°C		%	≈10

All information data are based on years of experience in production and operation of sealing elements. However, in view of the wide variety of possible installation and operating conditions one cannot draw final conclusions in all application cases regarding the behavior in gasket joint. The data may not, therefore, be used to support any warranty claims.



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